

COMMONWEALTH OF AUSTRALIA
DEPARTMENT OF CIVIL AVIATION



HANDBOOK
FOR
V.H.F. TRANSCEIVERS
PORTABLE & MOBILE

D.C.A. TYPE NOS. RT 12 & RT 13

VINTEN COMMUNICATION PRODUCTS PTY. LTD.
MELBOURNE AUSTRALIA

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1.0 BRIEF SPECIFICATION.

1.1 Classification.

The portable type RT12 and mobile type RT13 transceivers are designed to operate in the frequency band 118 to 132 Mc./S. Type RT12 operates from 230V 50 c/s A.C. and is intended for use where portability is required. Type RT13 operates from 12/24V D.C. and is designed primarily for operation in vehicles.

1.2 Composition and Type Numbers: RT12 Y5/672 RT13 Y5/673

DCA type RT12 corresponds to Vinten Type AMBTR8.

DCA type RT13 corresponds to Vinten Type AMMTR13.

Transceivers type RT12 and RT13 are executed in mono-unit construction with transmitter, receiver and power supply incorporated on a single chassis, designed to clip into ventilated snugly fitting cases, in a drawer type of construction.

Type RT12 is arranged to be fitted into a shock-mounted transit box with carrying handle for easy portability. In the case of type RT13, intended for vehicular service, the mounting case is intended to remain fixed in the vehicle, permitting rapid withdrawal of the complete unit for servicing or interchanging. Type RT13 is supplied with a combined plug-in power outlet fuse-board and a spring-mounted whip antenna.

1.3 Brief Description.

1.3.1 Transmitter.

The Transmitter is identical in both units. It is crystal controlled, Amplitude Modulated, mounted on the same chassis as the receiver, and is capable of being modulated 100% with an R.F. input to the antenna of 5 watts. The crystal frequency is multiplied twelve times to obtain the output frequency and all R.F. stages are transformer coupled to minimise spurious radiation. The modulator includes an efficient limiter and uses a low input variable reluctance microphone. Transmitter heaters are controlled by a microswitch mounted on the microphone cradle.

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1.3.2 Receiver.

The Receiver is identical in both units also. It is a double conversion superheterodyne, utilising one crystal for control. An efficient A.V.C. circuit, muting circuit and noise limiter are incorporated in the Receiver. Audio output, capable of a maximum 2½ watts, is applied to a 4" speaker mounted on the front panel. The mute and volume controls and on-off switch are also mounted on the front panel.

1.3.3 Power Supply.

The RT12 power supply is mounted on the same chassis as the transceiver and located across the rear section. It operates from 190-270 volts 50 c/s A.C. and is controlled by an on-off switch mounted on the front panel.

The RF13 power supply is also mounted on the same chassis as the transmitter and receiver and located across the rear section. It is a balanced transistorised converter and can be connected for 12V or 24V operation. The transistors are mounted on an extruded aluminium heat sink which is bolted to the rear of the chassis and protrudes through the rear of the case, ensuring adequate cooling.

N.B. THE TRANSISTOR POWER SUPPLY IS POLARITY SENSITIVE. INCORRECT POLARITY WILL RESULT IN DESTRUCTION OF THE TRANSISTORS.

1.3.4 Antenna.

A stub matched quarter wave whip antenna is supplied for mounting on metal-roofed vehicles. Construction is of all non-ferrous materials, chrome plated where necessary. A stainless steel compression spring with internal copper braid tail supports the whip section and provides a shock resistant assembly. A rubber gasket ring effectively precludes any chance of moisture leakage.

1.4 Power Requirements. (Typical Figures)

1.4.1 RT12.

Phases	One
Voltage	190 - 270
Frequency	50 C.P.S.
Power Consumed	Receive 72 watts Standby 100 watts Transmit 124 watts
Power Factor	0.92 approx.

1.4.2 RT13.

Voltage	12V D.C. or 24V D.C.
Polarity	POSITIVE OR NEGATIVE

AS SPECIFIED
(see 1.3.3)

Battery Amps.

	12V	24V
Receive	4	2.2
Standby	7	3.5
Transmit	8	4

1.5 Performance Specification:

1.5.1 Transmitter.

Radio Frequency Section: 5 stage crystal controlled.
Total multiplication twelve times.

Crystal Frequency: 9.83 - 11 Mc./S.

Crystal Tolerance: .0035%

Output Frequency: Single frequency in the band 118 - 132 Mc./S.

Power Output: 5 watts carrier to 70 ohm load from push pull Class C output stage.

Modulation: Plate and screen modulation of the final amplifier. Less than 5% distortion for 90% modulation with limiter operating.

Carrier Noise: Greater than 46 db below level corresponding to 100% modulation.

Frequency Response: ± 3 db 300-3000 c.p.s.

Spurious Radiations: All greater than 70 db below rated output.

1.5.2 Receiver.

Tuning Range: 118 - 132 Mc./S. crystal controlled.

Signal Frequency Section: 1 stage at above frequencies.

First Intermediate Frequency Section:

16.44 - 14.88 Mc./S.

Second Intermediate Frequency Section: 2 Mc./S.

Crystal Frequency: 12.888 - 14.44 Mc./S.

Crystal Tolerance: .0035%

Sensitivity: Audio output greater than 1 watt for 2 μ V input, modulated 30% at 1000 c.p.s.

Signal/Noise Ratio: Better than 12 db for 1 μ V input, modulated 30% at 1000 c.p.s.

<u>Audio Response:</u>	300	- 3db
	1000	0db
	2000	- 3db

1.5.2 (cont)

A.V.C. Output level does not vary by more than 5 db with an input variation of 5 μ V to 0.1 V.

Mute Control: May be set to operate at any R.F. input voltage between 0.25 μ V and 10 μ V. When the mute control is rotated fully anti-clock wise, the mute circuit is inoperative.

Selectivity: 2nd IF Channel

<u>Bandwidth</u>	<u>Attenuation</u>
\pm 25 Kc./S	4.5 dB
\pm 70 Kc./S	63 dB
\pm 100 Kc./S	120 dB

Distortion: Not greater than 5% at an RF input of 100 μ V and an audio output of 1 watt.

1.6 Electron Tube and Crystal Complement.

1.6.1 Electron Tube Complement.

Receiver.

Type	Circuit Ref.	Function
6AK5	V1	R.F. Amplifier
6AK5	V2	1st Mixer
6BA6	V5	2nd Mixer
6BA6	V6	I.F. Amplifier
6BA6	V7	I.F. Amplifier
6AU6	V8	I.F. Amplifier
6AV6	V9	Audio and A.V.C. Detector Audio Voltage Amplifier
6BW6	V10	Audio Power Output
6U8	V4	Crystal Oscillator Crystal Frequency Multip.
6AM6	V3	Frequency Multiplier
12AT7	V11	Mute Relay Control Tube
OA202	W1	Noise Limiter
OA202	W2	Noise Limiter
OA202	W3 W, S	Mute Circuit Noise Detector

1.6.1 (cont)

Transmitter:

Type	Circuit Ref.	Function
6U8	V12	Crystal Oscillator and Tripler
QQE03/12	V13	Doubler-Doubler
QQE03/12	V14	Class C Power Amplifier
12AT7	V15	Microphone Amplif.
6BA6	V16	Limiter Control Tube
12AT7	V17	Audio driver
QQE03/12	V18	Push-pull Modulator
OA202	W4	Limiter Diode

D.C. Power Supply:

2N1099 (DT80)	Q1	Balanced Push-pull DC-DC Convertors
2N1099 (DT80)	Q2	Balanced Push-pull DC-DC Convertors
1N1442	W5 W6 W7 W8	H.T. Rectifiers
1N1442	W9	Bias Rectifier

A.C. Power Supply:

1N2088	W10, 11 12, 13	H.T. Rectifiers
1N1442	W14	Bias Rectifier
1N1442	W15 W16	Relay Supply Rectif.

1.6.1 (cont)

Total quantity of Each TypeTransmitter & Receiver

Type	Total Number
6AK5	2
6AU6	1
6BA6	4
6AV6	1
6BW6	1
6U8	2
6AM6	1
12AT7	3
QQE03/12	3
OA202	4

D.C. Power Supply

2N1099 (DT80)	2
1N1442	5

A.C. Power Supply

1N1442	3
1N2088	4

1.6.2 Crystal Complement:

1 Receiver Crystal AT Cut in HC6U Holder
adjusted to 0.001% with a parallel capacity
of 20 PF.

1 Transmitter Crystal AT Cut in HC6U Holder
adjusted to 0.001% with a parallel capacity
of 20 PF.

1.7 Special Tools:

Two special tuning tools and one Allen Key are supplied with each transceiver, located in stowage clips on the chassis.

1. A nylon tool for capacitor adjustment.
2. A combination tool for use with I.F. transformers consisting of a slug tuning tool and a slug locking ring tool.
3. An Allen key for 5/32" grub screws in knobs.

1.8 Mechanical Construction and Dimensions.

Cases and chassis are constructed in 18 s.w.g. M.S. sheet. Perforated sheet is utilised for sides and bottom of the cases to provide adequate ventilation. The front panel and case, which is fabricated by spot welding, are secured together by two simple clips to form a flush fitting unit. The transistor heat sink is an aluminium extrusion.

Finish to surfaces are as follows :-

- (a) Chassis - Cadmium plated and passivated prior to screen printing.
- (b) Cases & Panels - Painted to standard D.C.A. Specifications.
- (c) Heat Sink - Heavily anodised black.
- (d) Fittings, Hardware, etc. - Chrome, Nickel or Cadmium, according to the end use.

The outside dimensions of the RT12 is 15" width x 13" depth x 8" height.

The outside dimensions of the RT13 is 14½" width x 11½" depth x 5¼" height.

Total weight, including all accessories, of the RT12 is 43 lbs.

Total weight, including all accessories, of the RT13 is 26 lbs.

2.0 TECHNICAL DESCRIPTION.

2.1 Receiver.

To facilitate a circuit description, the major circuit components are tabulated below.

<u>Section</u>	<u>Component</u>	<u>Function</u>
Signal Frequency	L1	Aerial Coil
	V1	6AK5 RF Amplifier
	T1	RF Transformer to V2
	V2	6AK5 RF mixer
	RL1	Change over relay
16-14 Mc./S.	T3	I.F. transformer to V5
	V5	Second mixer
2 Mc./S.	T6 T7	I.F. Transformer to V6
	V6	6BA6 I.F. Amplifier
	T8	I.F. Transformer to V7
	V7	6BA6 I.F. Amplifier
	T9	I.F. Transformer to V8
	V8	6AU6 I.F. Amplifier
	T10	I.F. Transformer to V9
	V9	Double diode detector & Audio Amplifier
Audio	V10	6BW6 Output Pentode
	W1 W2	Noise Limiter
Mute	V11	Mute Relay Control Tube
	W3	Mute Noise Diode
RF Oscillator	V4	6U8 Oscillator & Doubler
	T5	Tuned Oscillator Load for V4 Pentode
	T4	Doubling Transformer to V3
	V3	6AM6 Quadrupler
	T2	Tuned Quadrupling Load for V3.

2.1 (cont.)

Crystal Oscillator.

The Receiver is a double conversion type using one crystal as the source for deriving both converter frequencies. The second mixer utilises the crystal frequency while the first mixer utilises eight times the crystal frequency.

The crystal oscillator is a Colpitts type, using the screen grid of the pentode section of the 6U8 as an anode for the oscillator section and the plate of the pentode section as a point from which amplified oscillator voltage is obtained for the second mixer. T5 is a tuned load for the pentode. The grid anode connection prevents the crystal frequency changing due to detuning of any tuned circuit, normally present in other types of oscillator circuits. The crystal frequency is applied to the second mixer via C25. It is also applied via C21 to the grid of the triode section of the 6U8 which with T4 in the anode circuit doubles the crystal frequency. T4 also couples the doubled frequency to the grid of the 6AM6 quadrupler. T2 is the anode load of the 6AM6 and is tuned to eight times the crystal frequency. From the secondary of T2 this frequency is applied to the grid of the first mixer via C14.

T.P.2 is a test point for tuning T5, and T.P.3 permits the tuning of T4, using grid current in both cases as an indication.

R.F. and I.F. Stages.

The aerial feeder is connected, via changeover relay P.T.T. to the tapped coil L1. The R.F. input is then transferred to the grid of V1 via C2 where it is amplified before being applied to the first mixer via T1 and C13. In V2 the frequency is changed to that of the first I.F. (14.88 - 16.44 Mc./S.) and then applied to the second mixer via T3. In V5 the frequency is changed to that of the second I.F. (2 Mc./S.) The signal is then amplified in conventional manner in V6 V7 and V8 and applied to the double diode detector in V9.

The I.F. transformers T6, T7, T8, T9 and T10 are all identical and overcoupled to obtain a bandwidth of 25 Kc./S. at an attenuation of 4db.

2.1 (cont)

Detection and Audio Stages.

The I.F. frequency is applied to both diodes as in a conventional receiver. The A.V.C. diode (pin 6) does not conduct immediately but is delayed until the diode is at a potential more positive than the cathode of the triode which has cathode bias. The A.V.C. is filtered via R35, C54 and applied to V7, V6 and V1.

Audio detection takes place at diode 2 of V9, the diode load being R30 and R31. At the junction of R30 and R31 the audio is taken off and applied to the diode limiter W1, W2 and associated components R34, R33 and C59.

The junction of W2 and R34 is held at a negative voltage with respect to the cathode of V9 corresponding to the carrier level. Due to the time constant of R33, C59, this voltage cannot follow the audio impulse type noise.

When noise or any audio in excess of 100% modulation is received, the junction R30, R31, becomes more negative than the cathodes of the diodes W1, W2. The diodes cease to conduct under these conditions, thereby stopping the noise from reaching the audio amplifier.

The audio is fed from the junction of W2 and R34 via C61, R42 and R43 to the grid of V9. There it is amplified and fed to the audio output tube V10 for further amplification before being applied to the speaker.

Mute Circuit.

V11 is the mute relay control tube and the circuit is a simple form of codan. Audio signal, noise and a D.C. voltage proportional to the strength of the received signal is fed from terminal 4 of T10 via R32 to a network in the grid circuit of one triode of V11. C62 and R39 is a high pass filter which filters out both the D.C. voltage and the audio signal but lets the noise pass, via C63, to the diode W3. R40 and C64 is a low pass filter which filters out the audio signal and noise and permits the negative D.C. voltage to be applied to the grid. Meanwhile the noise voltage is rectified by diode W3 so that a positive voltage is formed tending to buck the negative voltage

2.1 (cont)

already applied to the grid and this causes more plate current to flow.

An adjustable trigger level is provided by R50 in the cathode of the 1st section of V11. R49 is a HT bleed resistor which assists in stabilizing this voltage. The adjustment of R50 determines the level of the applied signal which will open the mute relay. In the anode circuit of the same triode is a resistor of high value (R48) to produce a large voltage difference for grid voltage changes. This anode voltage is applied directly to the grid of the second triode. Cathode resistor R51 and HT bleed resistor R52 provide bias which is substantially independent of plate current until the grid voltage rises to the appropriate value, when plate current rises sharply and the relay operates, opening the mute contacts.

In the no signal condition, the second triode is nearly cut off while the first triode is conducting. An R.F. signal produces the negative D.C. voltage which tends to cut off the first triode and the subsequent rise in plate voltage causes the second triode to conduct and operate the mute relay.

In the absence of a signal, noise pulses cause the positive voltage mentioned above. This causes the first triode plate current to increase which cuts off the second triode. Hence noise will not unmute the receiver but rather tends to hold it muted. The application of a weak noisy signal combines both these operations and it is not until a readable signal to noise ratio is obtained that the mute opens.

The method of muting used is to bias the output tube V10 to cut off, in the muted condition the grid of V10 is biased to approximately -45 volts with respect to cathode, in the unmuted condition M1 contacts are closed, the bias then being reduced to -12.5 volts by the divider formed by R46 and R47.

2.2 Transmitter.

Radio Frequency Section.

<u>Tube</u>	<u>Function</u>	<u>Remarks</u>
V12		
6U8		
Pentode	Oscillator	
	Amplifier	
Triode	Tripler	
		Screen is utilised as plate of oscillator circuit and is electron coupled to plate circuit of V12A, giving an amplified voltage of frequency "f" which is transferred to V12B by T12. Output at 3f is transferred by T13 to V13A.
V13 QQE03/12	Doubler	Output at 6f is coupled via C99 to V13B.
Double Tetrode	Doubler	Output at 12f is coupled by T14 to V14. Output is balanced with respect to earth.
V14 QQE03/12	Push-pull	Modulated output at 12f is coupled into load by T15.
Double Tetrode	Power Amplifier	

Circuit Details.

The crystal oscillator is a Colpitts type which is identical to that used in the receiver. T12 couples the output of the oscillator-amplifier to V12B which with its transformer load (T13) triples the frequency. T13 also couples the signal to V13A which doubles the frequency in its load L2, C98. The output of V13A at 6f is coupled by C99 to V13B which also acts as a doubler. T14 selects the output of V13B at 12f and feeds it to V14 as a balanced signal to drive the push-pull power amplifier.

Screen and Anode modulation is used on V14 and the output is transferred to the feeder by T15. T15 is a double tuned transformer with the output tapped off the secondary. The R.F. passes to the aerial change over relay and via a high pass filter to the aerial socket. The low pass filter reduces harmonic radiations to a level less than -70db with respect to the carrier level.

2.2 (cont)

All the stages except the power amplifier have resistance capacity decoupling networks in the HT line.

Metering at TP5, TP6, TP7, TP8 and TP9 is provided for easy and direct tuning of each stage.

Fixed grid bias of approximately 25 volts is used on the final power amplifier to prevent the ratings of V14 being exceeded in the event of failure of grid drive.

2.3 Modulator:

<u>Tube</u>		
V15A ½ 12AT7	Microphone Amplifier	Low level input
V15B ½ 12AT7	Microphone Amplifier	Control voltage audio Amplifier
V16 6BA6	Limiter Amplifier	Constant output stage, controlled by bias volts via diode W4.
V17 12AT7	Driver	Phase splitter.
V18 QQE03/12	Push-pull Modulator	Class AB1 Output to modulation transformer T16.

Circuit Details:

The input stage V15A amplifies speech signal from a low level rocking-armature microphone. Cathode feedback is used in this stage. The output is coupled via C122 to V15B. A proportion of the output of V15A is not used for modulation purposes but is amplified by V15B and rectified by W4. A negative voltage is developed at the junction of R88, R89, R90 and C126. This negative voltage reduces the gain of V16 and as the voltage is proportioned at the audio level, limiting takes place. By adjusting R83 it is possible to maintain a high average level of modulation without overmodulating. The output from V16 is fed via C130 to V17 which is operating as a phase splitter and driver. Balanced output from V17 is fed to V18 via C132 and C133 to the modulator tube V18. Fixed bias is used on V18 and it operates in Class AB1. The output is fed to the modulation

2.3 (cont)

transformer, the secondary of which is in series with the HT supply to the power amplifier. A resistance network applies approximately 85% of the modulating voltage to the screen of the power amplifier. TP10 provides method of metering the modulator plate current.

Decoupling networks are provided in the HT line supplying V15 and V16 in order to reduce carrier noise.

2.4 Power Supply - RT12:

The RT12 power supply consists of a normal A.C. to D.C. supply. S3 is used in the primary of power transformer T18 for switching the receiver on and off. F2 protects the transformer against abnormally high currents and voltages.

The secondaries of T18 consist of the following winding and functions :-

- (a) A 6.3 volt winding for the receiver heaters.
- (b) A 6.3 volt winding for the transmitter heaters.
- (c) A 15 volt winding for relay operation which is applied to a full wave silicon rectifier, W15, W16, from which 12V D.C. is obtained to operate the aerial changeover relay. Both the 12V L.C. supply and transmitter heaters are controlled by S4 so that high tension cannot be applied to the transmitter in the absence of heater voltage.
- (d) A 50 volt winding for bias supply which is applied to a half wave rectifier circuit from which -50 volts D.C. bias for the power amplifier and modulator is obtained, each with its own resistance capacitance filter.
- (e) A 170/190 volt H.T. winding which supplies a bridge connected rectifier circuit of silicon diodes. 200 volts D.C. output is fed via a capacitance input filter to a springset on relay PTT so that high tension can be applied to either receiver or transmitter as required. A springset is also provided on the relay to change taps on the H.T. winding to maintain 200V D.C. under the differing load conditions of the receiver and transmitter.

2.5 Power Supply - RT13.

The Power Supply for RT13 is of recent design and employs transistors in place of vibrators. It is a balanced push-pull converter using Delco Transistors, type 2N1099 (DT80). Conversion from 12 volt operation to 24 volt operation is simply a matter of changing transformer connections and terminal connections on the terminal boards.

The principle of operation of the supply is that only one transistor is conducting at one time. A study of the circuit reveals that in switching off one transistor and switching on the other results in a reversal of flux in the transformer. This reversal of flux induces a voltage in the secondaries which can be rectified at a much higher voltage due to a step up turns ratio.

R113, R114 and R115 is a bias or starting arrangement so that the circuit will commence oscillation automatically upon removal of a short circuit, should one occur. The bias produced by the resistance network causes both transistors to conduct to a small degree. Owing to dissimilarity of characteristics of transistors or resistance values, one transistor will conduct more than the other (say Q1). This difference will create a resultant flux which includes a voltage in the feedback winding whose polarity is negative at the base of Q1 and positive at Q2. This tends to cause Q1 to pass more collector current and Q2 to tend to be cut off. This increases the voltage in the feedback winding and Q1 is switched on and Q2 is cut off. The current through Q1 and the associated winding rises till saturation is reached. At this point, due to the decrease in rate of change of current, the feedback voltage disappears and this tends to reduce the current already flowing through Q1. This decrease in current produces a feedback voltage which is negative at the base of Q2 and positive at the base of Q1. This results in a switching waveform as the current in Q1 drops to zero and Q2 is switched on. The cycle is then repeated at a frequency dependent on circuit constants etc; in this case approximately 600 c.p.s.

It will be noted that the positive lead is connected to the emitter and so we have a small positive bias on the emitter with respect to the base and a large negative bias on the collector with respect to the base.

2.5 (cont)

Reversing the polarity of the supply leads will result in a large positive bias on the collector and the resulting current will cause the instantaneous destruction of the transistors. Also earthing the base of the transistors will result in a large positive bias on the emitter. This will again result in destructive values of current in the transistor.

The secondary circuit is the same type as used in the RT12 with a bridge rectifier feeding a capacitor input filter. The excellent regulation of the transistor supply eliminates the need to change taps on the secondary in the transmit condition. Short circuits to earth in the high tension line will stop the converter oscillating but the heatsink and circuit values in the supply have been chosen so that a short circuit may be left on indefinitely without damaging any components.

3.0 INSTALLATION AND OPERATING INSTRUCTIONS.

3.1 Packaging:

The RT12 is packed as a single package 18" high x 15" wide x 9" deep. Gross weight 44 lbs.

The RT13 is also packed as a single package and is 19" high x 12 $\frac{3}{8}$ " wide x 6" deep. Gross weight 27 lbs.

It contains the transceiver, a DC outlet and fuse board and antenna with 12 ft. of co-axial cable and a connector.

3.2 Installation:

Transceiver.

When the transceiver is first unpacked it should be examined for any damage.

Unclip the case retaining catches and remove the unit from the case. Check that crystals and tubes are seated correctly in their sockets.

Select a mounting position in the vehicle so that it is convenient for the operator to reach the controls and microphone, and also to hear the speaker. Mount the case, using three or four $\frac{1}{4}$ " bolts, spring washers and nuts and any spacers, brackets, etc., as required for the particular vehicle and location of the set. Holes have to be drilled in the case to suit the conditions. Ensure that the case is now firm and free from distortion and is not likely to vibrate when the vehicle is passing over rough or corrugated roads. Drill one hole and mount the D.C. outlet and fuse board in a position close to the set so that the battery lead plug from the set can be plugged in. From the outlet board connect battery cables of size at least 162/.0076 to the battery terminals or between the starter solenoid and frame, using split type washers to ensure continued good connection. Insert a 10 amp. fuse for 12V sets and 5 amp. fuse for 24V sets.

Before replacing the chassis in the case, check that the unit is wired for the correct battery voltage and polarity. This information is contained on a

3.2 (cont)

warning plate on the battery leads. Should the polarity be incorrect this can be rectified by changing the connections on TS3 and TS2. The emitters of the transistors must be connected to the positive lead.

FAILURE TO OBSERVE CORRECT POLARITY WILL RESULT IN INSTANT DESTRUCTION OF THE TRANSISTORS.

Whenever the battery is removed after the transceiver is installed, every care should be taken to ensure that it is replaced with the same polarity.

Antenna.

The Antenna is supplied with a telescoping section to provide length adjustment and a stub which is to be cut to the correct length for the particular application. A chart is supplied at the rear of this handbook giving approximate lengths for stub and whip for various frequencies when the antenna is mounted centrally in the roof of a Holden Model F.C. Utility and is intended purely as a guide for this particular vehicle. It is essential that every installation be checked and adjustments to stub and whip lengths be made till a satisfactory standing wave ratio is obtained. This must be done with doors closed, bonnet down and no personnel within ten feet of the antenna using the transceiver as a signal source and the aerial mounted as stated below.

Select a central position for mounting the antenna. Drill a hole $1\frac{1}{2}$ " diameter in the roof taking care not to damage the lining. Using the split ring as a template, mark out and drill 4 holes each $5/32$ " diameter and two holes $\frac{1}{8}$ " diameter. Countersink the two $\frac{1}{8}$ " holes for the two 6EA screws which secure the split ring inside the roof of the vehicle. Scrape clean the under side of the roof which will make contact with the split ring. Insert the ring through the $1\frac{1}{2}$ " hole and fasten it to the underside using the two countersunk screws supplied. The braid of the co-axial cable feeder end stub must be tinned where it is held by the clamp at the aerial base. Feed the co-axial cable in the direction of the transceiver between the hood and the lining and bring it out at a point convenient for the particular vehicle.

3.2 (cont)

Insert the rubber "O" ring between the bottom of the antenna and the roof. Fasten the antenna to the roof using the four 4BA screws supplied. Screw the whip into the base. Pull the co-axial cable through ensuring that there are no sharp bends and after leaving ample spare cable, fix the connector to the cable. Screw the connector into the aerial socket.

The unit is now ready for putting into operation.

Checking Operating Conditions.

With the antenna connected to the transceiver, switch on the "on-off" switch and remove the microphone from the cradle on the front panel. Allow 20 seconds for the valves to warm up and then operate the press-to-talk button on the microphone and check the battery voltage appearing between the switch S1 and earth.

For 12V operation - minimum volts 11.8

For 24V operation - minimum volts 23.6

If the voltages measured are below those listed it is advisable to check that the battery is not discharged, and also check connections and cabling for excessive resistance.

Transmitter:

The output stage of the transmitter must be tuned to the antenna on the vehicle for maximum output. Connect a 0-100 mA meter to TP9. Using the special tuning tool provided, screw C107 anti-clockwise till its capacity is at a minimum. Tune C105 for a minimum plate current reading on the meter. Screw C107 in and tune it for a maximum of plate current. This maximum value should be 60 mA. If it is different from these values, adjust the coupling of T15 and retune C107 till the plate current is in the range 60 mA. The tuning of C107 must be the last adjustment, not the variation of T15 coupling. When this has been accomplished the transmitter is tuned to the aerial for 5 watts output.

3.2 (cont)

Receiver.

Rotate the mute control anti-clockwise and noise should be heard in the speaker. Check that the action of the volume control is normal. Rotate the mute control clockwise till the set is muted. There should still be $\frac{1}{4}$ of one turn left between the position of the control when the set mutes and the fully clockwise position. Check that the set unmutes on a signal. With no signal into the receiver, set the mute control so that the receiver is just muted. Advance the control approximately 20° clockwise. The receiver should then unmute on signals of less than $1\mu V$ strength.

3.3 Operation:

3.3.1 To Receive - RT12 RT13.

- (a) Switch the "On-Off" switch to "On" and the muting control to maximum anti-clock wise.
- (b) After approximately 20 seconds noise should be heard from the speaker.
- (c) Reset muting control till the noise disappears.

The receiver is now ready to receive messages. The receiver volume may be adjusted by the VOLUME control.

3.3.2 To Transmit:

RT13 - Remove the microphone from the cradle on the front panel. This switches on the transmitter heaters. After 30 seconds press the button on the microphone case and speak.

When speaking into the microphone, use a normal speaking voice and hold the microphone approximately three inches away from the lips.

Note: No transmission can take place until approx. 30 seconds after the microphone is lifted from the cradle. This arrangement reduces the battery drain and lowers the operating temperature of the equipment.

RT12 - The method of transmitting with the RT12 is basically the same as for the RT13. A separate TRANSMITTER FILS. ON switch is provided which must be manually operated 30 seconds before commencing to transmit.

4.0 MAINTENANCE

4.1 Tables of Voltages and Currents:

4.1.1 Power Supply Voltages:

Operating Voltage	Heater Volt-ages	H.T. Volts		Bias Volts at TP8		Bias Volts at Jetn. R100 R101	
		Rec-eive	Trans-mit	Rec-eive	Trans-mit	Rec-eive	Trans-mit
12.6 DC.	6.3	220	215	25	34	20	21
25.2 DC.	6.3	220	215	25	34	20	21
230 AC.	6.3	220	210	25	34	20	21

4.1.2 Power Supply Currents:

Operating Voltage	Battery Current A		High Tension Current mA	
	Transmit	Receive	Transmit	Receive
12.6 DC	8	4	160	130
25.2 DC	4	2	160	130
230AC.	-	-	160	130

4.1.3 Receiver Voltage Table:

Volume Control	Fully anti-clockwise
Mute Control	Fully anti-clockwise
R.F. Input	Zero
H.T. Supply	220 volts
Heater Volts	6.3 volts

Meter. Measurements marked V.V read with valve voltmeter. All others on instrument with 1000 Ω/V sensitivity.

4.1.3 Receiver (cont)

Valve No.	Pin 1	Pin 2	Pin 3	Pin 4	Pin 5	Pin 6	Pin 7	Pin 8	Pin 9
1	-	-	-	6.3	60	60	-	-	-
2	1.5VV	-	12.6	6.3	90	90	-	-	-
3	50VV	-	-	6.3	210	-	160	-	-
4	150	6VV	85	6.3	-	50	-	-	15VV
5	.5VV	4	6.3	12.6	120	120	4	-	-
6	.5VV	-	6.3	12.6	175	75	.5	-	-
7	.5VV	-	6.3	12.6	200	75	.5	-	-
8	-	4	0	6.3	220	160	4	-	-
9	9VV	10	0	6.3	7VV	-3	150	-	-
10	0	9	0	6.3	12.6	220	240	120	-
11	150	40	85	0	0	40	4.5VV	8VV	6.3

4.1.4 Transmitter Voltage Table.

Unmodulated output 5W HT 220V

Valve	Plate		Screen		Grid		Cathode	
	Pin	Volts	Pin	Volts	Pin	Volts	Pin	Volts
V12A 6U8	6	100*	3	75*	2	6VV	7	0
V12B 6U8	1	150*	-	-	9	34*	8	2.5
V13A QQE03/12	8	160*	7	85	3	40*	2	0
V13B QQE03/12	6	160*	7	85	1	30W	2	0
V14 QQE03/12	6	220*	7	160	1 3	60*	2	0

* These readings were measured between decoupled points and earth.

4.1.5 Modulator Voltage Table.

Valve	Plate		Screen		Grid		Cathode	
	Pin	Volts	Pin	Volts	Pin	Volts	Pin	Volts
V15A 12AT7	6	70	-	-	7	0	8	1
V15B 12AT7	1	65	-	-	2	0	3	1
V16 6BA6	5	35	6	30	1	0	7	0
V17 12AT7	1	110	-	-	2	20VV	3	23
	6	110	-	-	7	20VV	8	23
V18 QQE03/12	6	220	7	220	1	21VV	2	0
	8	220				21VV		

4.1.6 Receiver Test Point Readings.

✓ 300 µA METER;

Position	Current	
		+ 16µA
TP1		
TP2	1 mA	0.7 mA
TP3	1 mA	0.4 mA
TP4	10 mA	6.5 mA

4.1.7 Transmitter Test Point Readings.

HT 220V Output 5W unmodulated.

Position	Current	
TP5	10 mA	1.0 mA
TP6	1 mA	0.7 mA
TP7	10 mA	1.1 mA
TP8	10 mA	2.5 mA
TP9	100 mA	60 mA
TP10	100 mA	30 mA *

* rises to
60 mA at
100% mod.

4.2 Maintenance Adjustments and Alignments:

4.2.1 Receiver Alignment.

Test Equipment required -

- (a) $50\mu A$ Amp centre zero meter.
- (b) Signal Generator covering 2 Mc./S.
- (c) Signal Generator covering the range 118 - 132 Mc./S.
- (d) Resistor 15K ohms. with clips.
- (e) 0-~~100~~ μA meter.

2 Mc./S. I.F. Alignment.

Plug the $50\mu A$ Amp. meter into T.P.1 so that the meter deflects to the positive side of the scale with no signal. Connect the generator between Pin 1 of V8 and ground at 2 Mc./S. and full output. Using the special aligning tool provided, unlock the top and bottom slugs of T10 and tune for a maximum deflection on the meter. Ensure that the slugs are tuned to the first maximum when starting with the slugs at the outer position. Reduce the output of the generator till the deflection is $-10\mu A$. Amps. Retune each slug and lock, only very slight pressure on the locking ring is necessary to satisfactorily lock the slug.

Connect the generator to Pin 1 of V7 and earth. Connect the 15K loading resistor across terminals 1 and 2 of T9.

Using the same tuning technique as described above, tune both slugs of T9 for maximum deflection, reducing the output of the generator to give $-10\mu A$ before giving the slugs a final tune and lock.

Connect the generator between Pin 1 of V6 and earth. Connect the 15K loading resistor between terminals 1 and 2 of T8. Tune both slugs of T8. Connect the generator between Pin 1 of V5 and earth. Connect the loading resistor between terminals 1 and 2 of T7. Tune both slugs of T7 as for T9. Disconnect the generator and resistor. (*) The I.F. Alignment is now complete.

* It is not necessary to align the I.F. alignment if the oscillator alignment has been done correctly.

4.2.1 (cont)

R.F. Alignment on Change of Frequency.

Select the crystal for the desired carrier frequency.

$$\text{Crystal Frequency} = \frac{\text{Carrier Freq. Mc./S}}{9} - 2 \text{ Mc./S}$$

Plug in the crystal. Plug in the 0-10 μ A meter into TP2. Tune both slugs of T5. Tune the top slug first for a maximum on the meter. Then tune the bottom slug for a minimum. Lock both slugs after tuning. The meter reading should be approximately 1 A. Shift the meter into TP3 and tune both slugs of T4 for a maximum, approximately [REDACTED].

Connect the V.H.F. Signal Generator to the aerial socket and apply full output voltage (0.5 volts if available). Set the Signal Generator by the calibration to the approximate carrier frequency. Vary the frequency till a tuning indication is given on the 50 μ Amp. meter in TP1. Tune the Signal Generator for maximum deflection.

Using the special tool provided, tune C1, C5, C6, C8 and C9 from the minimum capacity position for maximum meter deflection, taking care that the generator output is reduced at each tuning for a maximum meter deflection of + 10 μ A.

Having tuned the capacitors, check that the generator is exactly on the carrier frequency by tuning it for maximum deflection of the test meter. Retune C1, C5, C6, C8 and C9 if necessary again limiting the meter deflection to 10 μ A by reducing generator output. Now tune both slugs of T3 for maximum deflection, reducing the output of the generator to keep the maximum meter deflection down to +10 μ A.

The Receiver is now aligned and the generator output should be about 0.5 μ V. Give a final touch to the generator frequency, the slugs of T3, capacitors C1, C5, C6, C8 and C9 in that order. C5 and C6 can tune to spurious responses when the generator is set to outputs greater than 10 μ V and the original instruction to tune all condensers from the minimum capacity position should be adhered to.

A.B.
[REDACTED]

4.2.2 Transmitter Alignment.

$$\text{Crystal Frequency} = \frac{\text{Carrier Frequency}}{12 \text{ Mc./S.}}$$

Plug in the crystal. Connect RF Power Output Meter or matched antenna to antenna socket.

Plug in the ~~100~~¹⁰ mA meter into T.P.5. Press P.T.T. button on the microphone.

Tune the bottom slug of T12 for maximum deflection.

Tune the top slug of T12 for maximum deflection. The meter reading should be approximately. Reduce this reading by ~~10~~¹⁰ μ A by screwing top slug of T12 in.

Plug the meter into TP6.

Tune both slugs of T12 for maximum deflection, approximately.

Plug the meter into TP7.

Tune C98 for maximum approximately ~~7 1/2~~⁷ W. ~~100~~¹⁰ mA.

Tune C102 for a minimum.

Plug a ~~100~~¹⁰ mA meter into TP8.

Tune C102 and C103 for maximum approx. ~~20~~²⁰ W. ~~100~~¹⁰ mA.

Plug a 0-100 mA meter into TP9.

Screw C107 out to minimum capacity.

Tune C105 for a minimum approx. 20 to 30 W. ~~100~~¹⁰ mA.

Tune C107 for a maximum. Reading should be 60 W. ~~100~~¹⁰ mA.

If this reading is not obtained, adjust the coupling of T15 and retune C107. Repeat until the reading is 60 W. ~~100~~¹⁰ mA. The power output should be 5 watts. The power output stage must be tuned to the antenna when the set is returned to operation. (See Installation Instructions).

4.2.3 Checking Transmitter Audio Limiter.

Connect an audio generator with an output impedance of 600 ohms to an unbalanced attenuator using screened and insulated cable, then from the attenuator to terminal 1 and 2 on TS1 on the transceiver using screened and insulated cable. Earth the screen of the cable at terminal 2 on TS1 only. With an input to the transceiver of -35dBm at 1,000 cycles, adjust the modulation to approximately 50% by rotating the mod. set control R83.

Reduce the input to -45dBm then increase the input to -25dBm, between these limits the modulation percentage should not change by more than 2 db., if a greater variation results the limited amplifier valve V16, (6BA6) should be replaced and the test repeated.

Readjust the modulation to 100% with an input of 35 dBm.

5.1

Receiver.

5. COMPONENT SCHEDULE.

Circuit Code	Component Description	Function	DCA Ident No.	Manufacturer & Designation
Resistors:				
R1	100KΩ ± 10% 1W	V1 Grid	Y8/5492	IRC BTS
R2	27KΩ ± 10% 1W	HT Decoupling	Y8/6493	IRC BTB
R3	3.3KΩ ± 10% 1/2W	HT Decoupling	Y8/5474	IRC BTS
R4	47KΩ ± 10% 1/2W	V3 Screen	Y8/5488	IRC BTS
R5	1000Ω ± 10% 1/4W	TP3 Shunt	Y8/5463	IRC BTS
R6	1MΩ ± 10% 1/4W	V2 Grid	Y8/5504	IRC BTS
R7	100KΩ ± 10% 1/4W	V3 Grid Return	Y8/5492	IRC BTS
R8	10KΩ ± 10% 1/2W	HT Decoupling	Y8/167	IRC BTA
R9	4.7KΩ ± 10% 1/4W	HT Decoupling	Y8/5476	IRC BTS
R10	27KΩ ± 10% 1/4W	V4 Triode Grid	Y8/5485	IRC BTS
R11	1000Ω ± 10% 1/4W	TP2 Shunt	Y8/5468	IRC BTS
R12	1000Ω ± 10% 1/4W	V5 Cathode Bias	Y8/5463	IRC BTS
R13	47KΩ ± 10% 1/2W	HT Decoupling	Y8/168	IRC BTA
R14	100KΩ ± 10% 1/4W	V4 Pentode Grid	Y8/5492	IRC BTS
R15	47KΩ ± 10% 1/2W	V4 Screen Load	Y8/168	IRC BTA
R16	4.7KΩ ± 10% 1/2W	HT Decoupling	Y8/160	IRC BTA
R17	100KΩ ± 10% 1/4W	AVC Decoupling	Y8/5492	IRC BTS
R18	100KΩ ± 10% 1/4W	V6 AVC Grid return	Y8/5492	IRC BTS
R19	47Ω ± 10% 1/4W	V6 Cathode	Y8/5452	IRC BTS
R20	39KΩ ± 10% 1/4W	V6 Screen	Y8/5487	IRC BTS
R21	100KΩ ± 10% 1/4W	V7 AVC Grid return	Y8/5492	IRC BTS
R22	1000Ω ± 10% 1/2W	HT Decoupling	Y8/159	IRC BTA
R23	47Ω ± 10% 1/4W	V7 Cathode	Y8/5452	IRC BTS

5.1 Recipient: (cont.)

Part No.	Description	Function	Ident No.	Manufacturer & Designation
R24	Resistor, S.	V7 Screen Decoupling	Y8/5487	LAC BTS
R25	1000 Ω $\pm 10\%$ 1/4W	V8 Decoupling	Y8/839	Ducon RUV5J
R26	1000 Ω $\pm 10\%$ 1/4W	V8 Cathode	Y8/5468	LAC BTS
R27	39K Ω $\pm 10\%$ 1/4W	V8 Screen	Y8/5487	IRC BTS
R28	1000G $\pm 10\%$ 1/4W	HP Decoupling	Y8/839	IRC BTS
R29	470K Ω $\pm 10\%$ 1/4W	HP2 Feed	Y8/5500	IRC BTS
R30	47K Ω $\pm 10\%$ 1/4W	Diode Load	Y8/5488	IRC BTS
R31	27K Ω $\pm 10\%$ 1/4W	Diode Load	Y8/5488	IRC BTS
R32	47K Ω $\pm 10\%$ 1/4W	Mute Decoupling	Y8/5488	IRC BTS
R33	330K Ω $\pm 10\%$ 1/4W	Noise Filter	Y8/5498	IRC BTS
R34	330K Ω $\pm 10\%$ 1/4W	Noise Filter	Y8/5498	IRC BTS
R35	470K Ω $\pm 10\%$ 1/4W	A•V•C. Filter	Y8/5500	IRC BTS
R36	470K Ω $\pm 10\%$ 1/4W	A•V•C. Load	Y8/5500	IRC BTS
R37	1.5K Ω $\pm 10\%$ 1/4W	V9 Cathode Bias	Y8/5470	IRC BTS
R38	10K Ω $\pm 10\%$ 1/4W	V9 Cathode A.V.C. Delay	Y8/5480	IRC BTS
R39	150K Ω $\pm 10\%$ 1/4W	Mute Filter	Y8/5494	IRC BTS
R40	11K Ω $\pm 10\%$ 1/4W	Mute Filter	Y8/5504	IRC BTS
R41	10K Ω $\pm 10\%$ 1/4W	Minimum Volume	Y8/5480	IRC BTS
R42	220K Ω $\pm 10\%$ 1/4W	Audio HF Filter	Y8/5496	IRC BTS
R43	250K Ω $\pm 10\%$ 1/4W	Volume Control	Y8/5526	Morganite RVE
R44	1K Ω $\pm 10\%$ 1/4W	= V11 Grid	Y8/5504	IRC BTS
R45	47K Ω $\pm 10\%$ 1/4W	V9 Anode	Y8/5483	IRC BTS
R46	470K Ω $\pm 10\%$ 1/4W	V10 Bias	Y8/5500	IRC BTS
R47	150K Ω $\pm 10\%$ 1/4W	V10 Bias	Y8/5494	IRC BTS
R48	11K Ω $\pm 10\%$ 1/4W	V11 Anode	Y8/5504	IRC BTS
R49	220K Ω $\pm 10\%$ 1/4W	Voltage Divider	Y8/5496	IRC BTS
R50	10K Ω $\pm 10\%$ 1/4W	Cathode 1 of V11 Mute Control	Y8/60	Morganite RVE

5.1 Receiver (cont.)

Cir- cuit Code	Component Description	Function	DCA Ident. No.	Manufacturer & Designation
Resistors.				
R51	47KΩ ± 10% 1/2W	Voltage Divider	Y8/168	IRC BTA
R52	10K ± 10% 1/2W	Cathode 2 of V11	Y8/167	IRC BTA
R53	270Ω ± 10% 1/4W	2P4 Shunt	Y8/5461	IRC BTS
R54	1MΩ ± 10% 1/4W	V11 Grid	Y8/5504	IRC BTS
R55	47KΩ ± 10% 1/4W	Mute HF Compensation	Y8/5452	IRC BTS
R56	470KΩ ± 10% 1/4W	Mute HF Compensation	Y8/5500	IRC BTS
R57	1KΩ ± 10% 1/4W	V2 Screen	Y8/5463	IRC BTS
<i>Varactors.</i>				
R1S1	1.5Kvar	Varactor	Y8/317777	

S.1 Receiver (cont.)

Circuit Code	Component Description	Function	DCA Ident. No.	Manufacturer & Designation
<u>Coils and Transformers.</u>				
T8	Transformer	I.F.	Y9/1331	Vinten 135
T9	Transformer	I.F.	Y9/1331	Vinten 135
T10	Transformer	I.F.	Y9/1331	Vinten 135
T11	Iron core	Audio Output	Y9/1330	Vinten G9S
<u>Miscellaneous.</u>				
TP1	Crystal Socket	Crystal Socket	V8/511	Teletron SC22GP
TP2	Metering Socket	Detector Diode	V8/302	Teletron SC12LB
TP3	Metering Socket	Doub. Grid	V8/302	Teletron SC12LB
TP4	Metering Socket	Quad. Grid	V8/302	Teletron SC12LB
M/2	Loudspeaker 4 nd d.	Relay	Y12/977	Teletron SC12LB
	10,000 ohm 600			Rola 4C01
	t-type relay			
	Whip Antenna	Mutings	V13/1337	G.E.C.
	Co-axial cable		Y4/207	Vinten
	Plug co-axial		V5/1388	Melcon PT.11
			V8/19	Melcon 5B50868

5,4 D.C. Power Supply Unit

Circuit Code	Component Description	Function	DCA Ident No.	Manufacturer & Designation
<u>Resistors</u>				
R109	10Ω ± 5% 1½W	Q1 Base	Y8/877	Ducon RWV3J
R110	10Ω ± 5% 1½W	Q2 Base	Y8/877	Ducon RWV3J
R111	25Ω ± 5% 3W	Heater Balance	*Y8/900	Ducon RWV4J
R112	9.4Ω ± 5% 1ΩW	Heater Balance	Y8/6581	Ducon RWV5J
R113	3Ω ± 10% 1.5W	Q1 and Q2 Bias	Y8/6580	Ducon RWV3J
R114	400Ω ± 10% 1.5W	Q1 and Q2 Bias	Y8/6579	Ducon RWV3J
R115	200Ω ± 10% 1.5W	Q1 and Q2 Bias	Y8/5867	Ducon RWV3J
R116	100Ω ± 10% 1.5W	Relay Dropper	Y8/833	Ducon RWV3J
R117	4.7KΩ ± 10% 1/4W	V14 Bias Filter	Y8/5476	IRC BTS
R118	10KΩ ± 10% 1/4W	V18 Bias Filter	Y8/5480	IRC BTS
R119	10KΩ ± 10% 1/4W	V18 Bias Bleed	Y8/5480	IRC BTS
R120	6.3KΩ ± 10% 1/4W	V14 Bias Bleed	Y8/5478	IRC BTS
<u>Capacitors</u>				
C135	330pf ± 20% 500VW	V14 RF Bypass	*Y1/83	Ducon CDS HIK
C136	2200pf GMV 500VW	V15 RF Bypass	Y1/2236	Ducon CDS HIK
C137	2200pf GMV 500VW	PTP Relay Bypass	Y1/2236	Ducon CDS HIK
C138	25μF 50VW	Suppressor	Y1/2232	Ducon ET2CT
C139	16μF 450VW	HP Filter	Y1/2235	Ducon ET5CT
C140	16μF 450VW	HP Filter	Y1/2235	Ducon ET5CT
C141	25μF 50VW	V13 Bias Filter	Y1/2232	Lucon ET2CT
C142	25μF 50VW	V14 Bias Filter	Y1/2232	Ducon ET2CT
C143	50μF 125VW	V10 Bias Filter	Y1/2212	Ducon EM4DI
C144	2200pf GMV 500VW	PTP Relay Bypass	Y1/2236	Ducon CDS HIK
C145	2200pf GMV 500VW	V13 Millerant Bypass	Y1/2236	Ducon CDS HIK
C146	.02μF 750VW	Buffer	Y1/457	Ducon MP712

* DCA Replacement Item, *457.

5.4 I.C. Power Supply (cont.)

Circuit Code	Component Description	Function	DCA IDEN. NO.	Manufacturer & Designation
<u>Diodes & Transistors</u>				
Q1	Transistor	D.C. Converter	Y11/895	Delco 2N1099
Q2	Transistor	D.C. Converter	Y11/893	Delco 2N1099
W5	Silicon Diode P.I.V.400	HT Rectifier	Y11/867	Sarkes Tarzian 1M1442
W6	Silicon Diode P.I.V. 400	HT Rectifier	Y11/867	Sarkes Tarzian 1M1442
W7	Silicon Diode P.I.V. 400	HT Rectifier	Y11/867	Sarkes Tarzian 1M1442
W8	Silicon Diode P.I.V. 400	HT Rectifier	Y11/867	Sarkes Tarzian 1M1442
W9	Silicon Diode P.I.V.400	Bias Rectifier	Y11/867	Sarkes Tarzian 1M1442
<u>Coils, Chokes and Transformers</u>				
L5	RF Choke - filament	V15 Heater	Y3/NIV	Vinten 154
L6	RF Choke - LF	Converter supply	Y3/NIV	Vinten 153
L7	Not used			
L8	Choke 2H, 200mA	HF Filter	Y3/1519	A & R Type 3021
T17	Transformer DC Converter	DC Converter	Y9/1337	A & R Type 1914

5.4 D.C. Power Suppl V RT13 (cont.)

Circuit Code	Component Description	Function	DCA Ident No.	Manufacturer & Designation
<u>Miscellaneous.</u>				
S1	2 pole switch	LT Power	V14/621	Cutler Hammer 7320K3
S2	Micro switch	Tx Heaters	V14/925	Bellco V3
PMT P T S	Relay 1000 3CO Contacts	HT & Aerial Changeover	V13/1336	7R/3 (12V) Relays P/L.
F1	Fuse (for value see install. instructions)	DC Converter	V12/3	3AG
PL1	Pilot Lamp 10-28V	Receive Pilot	V1/298	Philips 10-28V Type 12006N
PL2	Pilot Lamp 10-28V	S/B Pilot	V1/298	Philips 10-28V Type 12006N
	D.C. Outlet & Fuse Board		V15/342	Vinten
	Switch Parts, Cradle. Part of Micro Switch Assy.		V14/1269	Vinten
	Tools, Aligning for I.P. Transformers		DIH/106	Vinten
	Tools, Aligning for Trimmer Conds.		DIH/105	Vinten

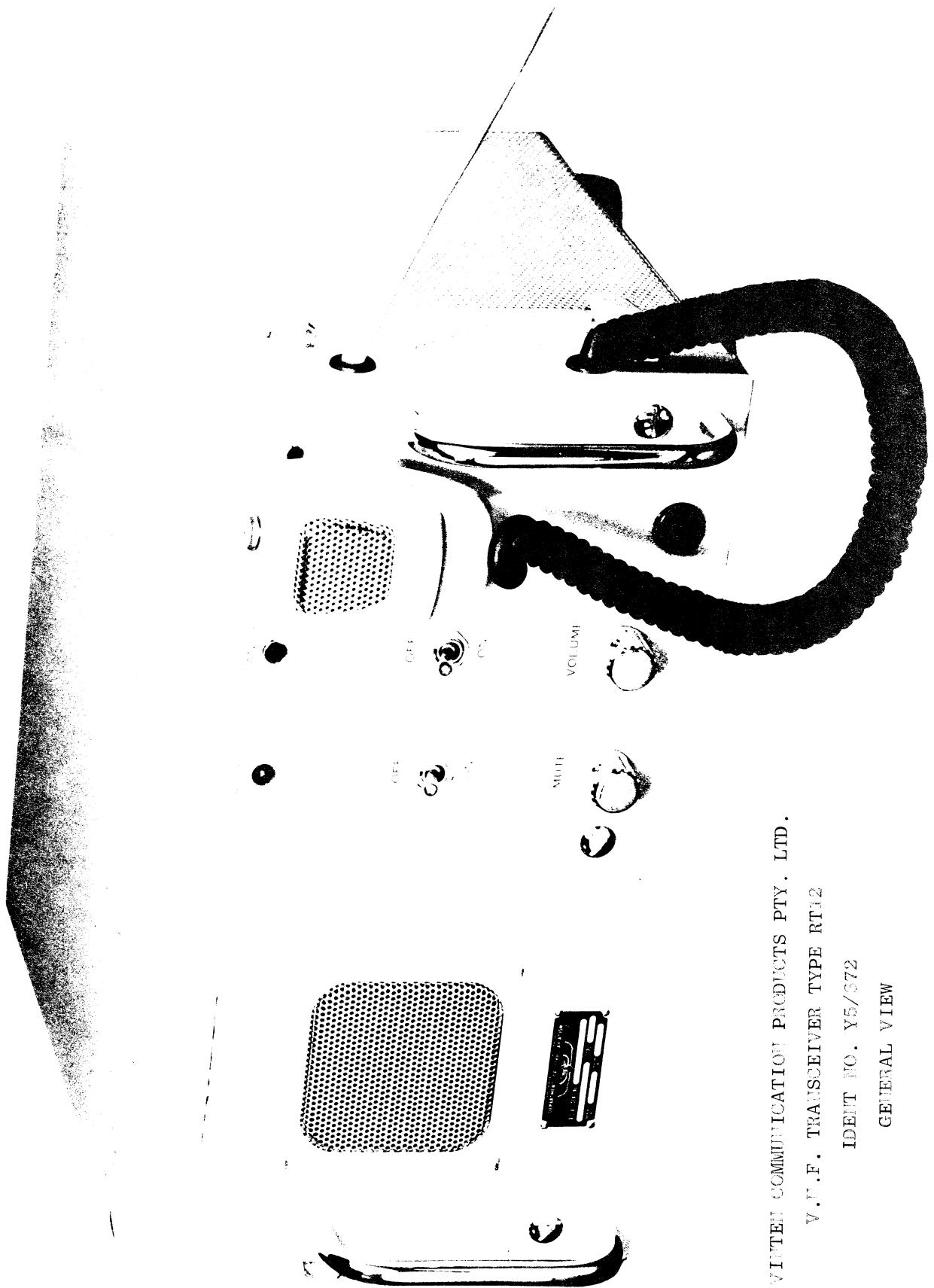
5.5 A.C. Power Supply RT12.

Circuit Code	Component Description	Function	DCA Ident No.	Manufacturer & Designation
<u>Resistors.</u>				
R121	4.7KΩ ±10% 1W	V14 Bias Filter	Y8/5476	IRC BTS
R122	10KΩ ±10% 1W	V18 Bias Filter	Y8/5480	IRC BTS
R123	10KΩ ±10% 1W	V18 Bias Bleed	Y8/5480	IRC BTS
R124	6.8KΩ ±10% 1W	V14 Bias Bleed	Y8/5478	IRC BTS
R125	20KΩ ±10% 1W	V10 Bias Feeder	Y8/5484	IRC BTS
<u>Condensers.</u>				
C147	16μF 450VW	HF Filter	Y1/2235	Ducon ET6CT
C148	16μF 450VW	HF Filter	Y1/2235	Ducon ET6CT
C149	25μF 50VW	V18 Bias Filter	Y1/2232	Ducon ET2CT
C150	25μF 50VW	V14 Bias Filter	Y1/2232	Ducon ET2CT
C151	100μF 25VW	PTT Supply Filter	Y1/2233	Ducon ET4DT
C152	330pF ±20% 500VW	V14 RF Bypass	*Y1/83	Ducon CDS HIK
C153	2200pF GMV 500VW	V15 RF Bypass	Y1/2236	Ducon CDS HIK
C154	50μF 125VW	V10 Bias Filter	Y1/2212	Ducon ET4DT
C155	2200pF GMV 500VW	V13 Heater Bypass	Y1/2236	Ducon CDS HIK

* DCA Replacement Item.

5.5 A.C. Power Supply R112 (cont.)

Circuit Code	Component Description	Function	DCA Ident. No.	Manufacturer & Designation
<u>Diodes.</u>				
W10	Silicon Diode PIV600	HP Rectifier	*Y11/899	Sarkes Tarzian 60K
W11	Silicon Diode PIV600	HP Rectifier	*Y11/899	Sarkes Tarzian 60K
W12	Silicon Diode PIV600	HP Rectifier	*Y11/899	Sarkes Tarzian 60K
W13	Silicon Diode PIV600	HP Rectifier	*Y11/899	Sarkes Tarzian 60K
W14	Silicon Diode PIV400	Relay Rectifier	Y11/867	Sarkes Tarzian 1N1442
W15	Silicon Diode PIV400	Relay Rectifier	Y11/867	Sarkes Tarzian 1N1442
W16	Silicon Diode PIV400	Relay Rectifier	Y11/867	Sarkes Tarzian 1N1442
* DCA Replacement Item.				
<u>Coils, Chokes, Transformers.</u>				
L9	Choke 1OH, 200mA	HT Filter	Y3/1520	A & R Type 3023
L10	RF Choke Filament Transformer	V15 Heater	Y3/HIV	Vinten 154
T18	190-270VAC	Power Supply	Y9/1338	A & R Type 1960
<u>Miscellaneous.</u>				
S3	2 pole switch	AC Power	V14/621	Cutler Hammer 732OK3
S4	2 pole switch	TX Heaters	V14/621	Cutler Hammer 732OK3
PPT 3	Relay 100Ω 3CO	HT. Aerial Changeover	V13/1336	Relays Pty.Ltd. Type 7R/3 (12V)
	Contacts	AC Mains	V12/3	2A Type 3AG
R2	Fuse 3AG	Receive Pilot	V1/33	Philips 6V MBC
PL3	Pilot Lamp	S/B Pilot	V1/33	Philips 6V MBC
PL4	Pilot Lamp			
Motor electric induction shaded pole 35 watt, 220-230V A.C. 0.1SA, 50 C.P.S., with fan blade Cooling				
			V4/527	Warner Drayton Product 15



V.I.T.E.T COMMUNICATION PRODUCTS PTY. LTD.

V.H.F. TRANSEIVER TYPE RT12

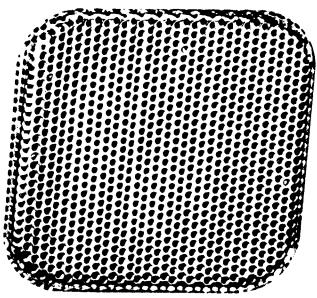
IDENT NO. Y5/572

GENERAL VIEW

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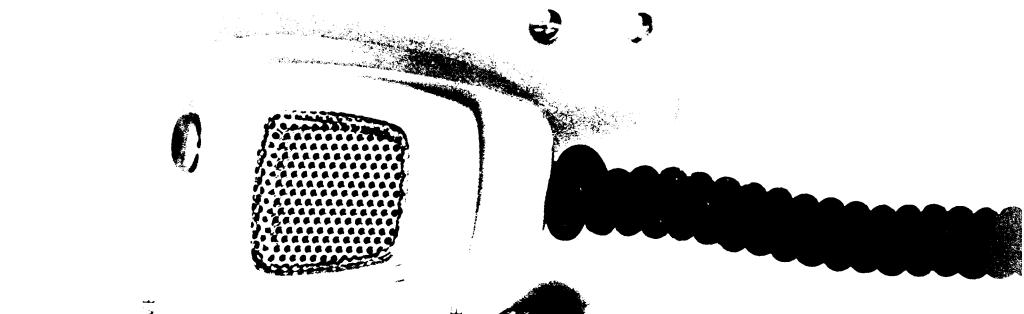


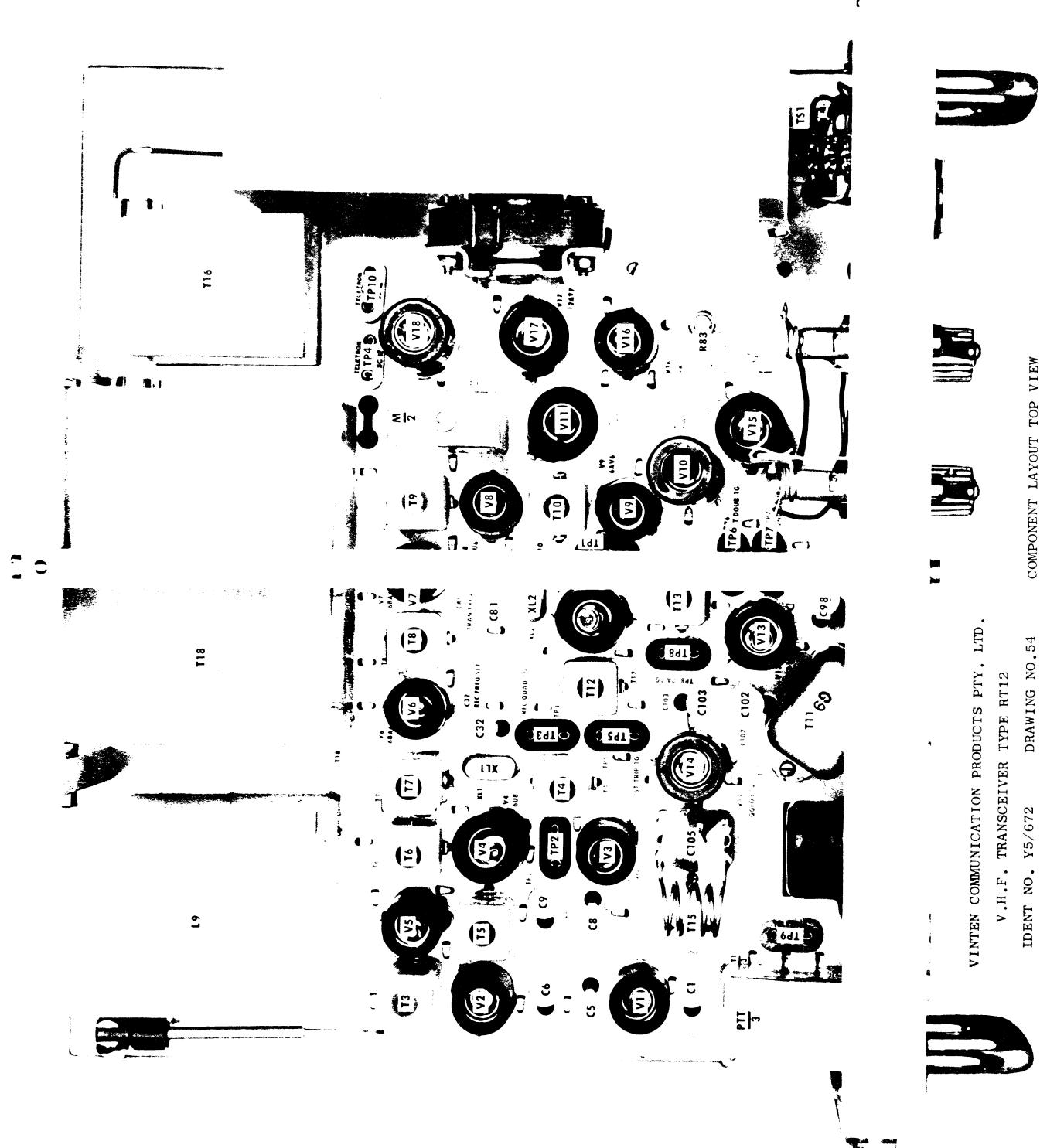
VINTEN COMMUNICATION PRODUCTS PTY. LTD.

V.T.F. TRANSCEIVER TYPE RT13

IDENT NO. Y5/473

GENERAL VIEW





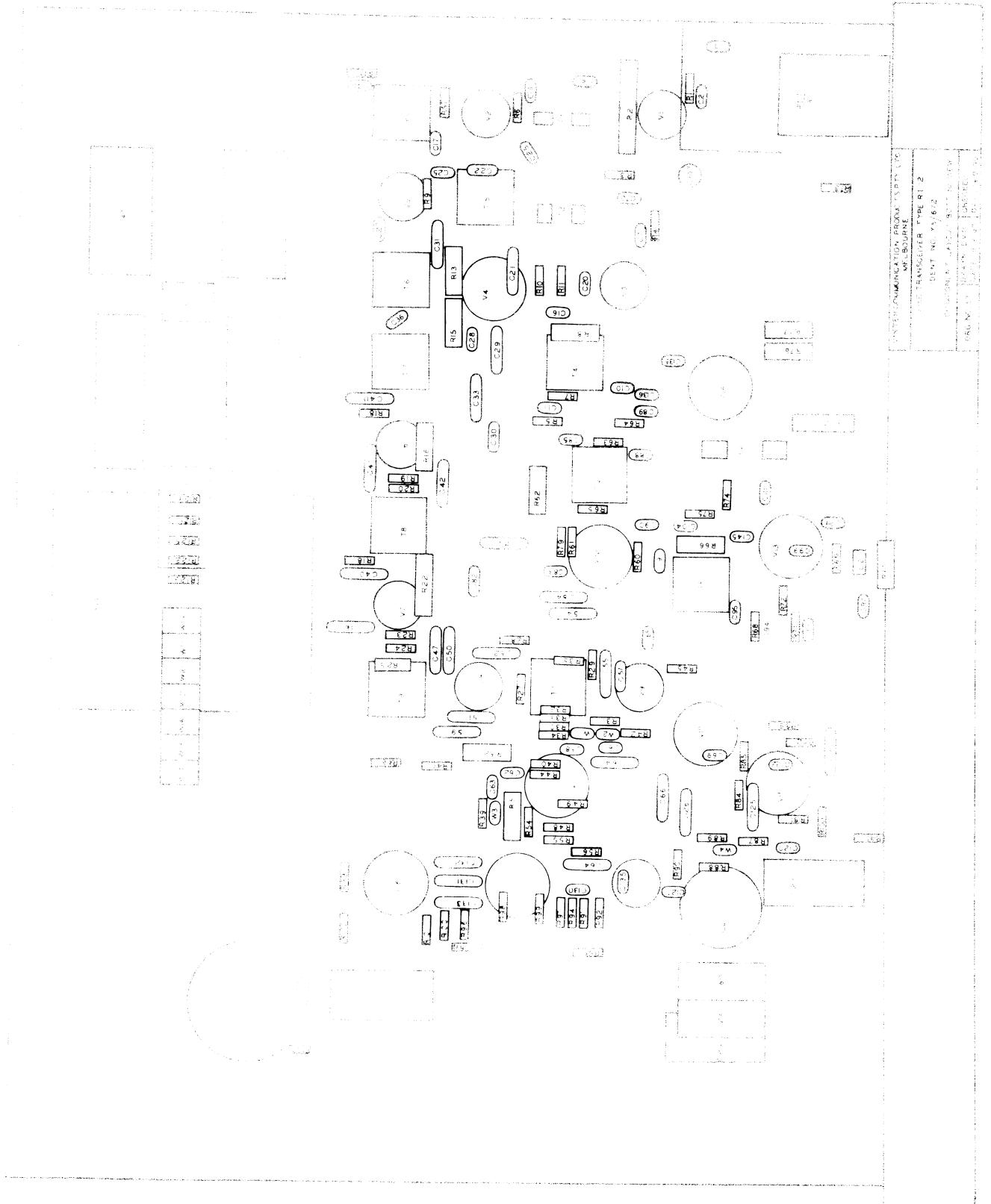
VINTEN COMMUNICATION PRODUCTS PTY. LTD.

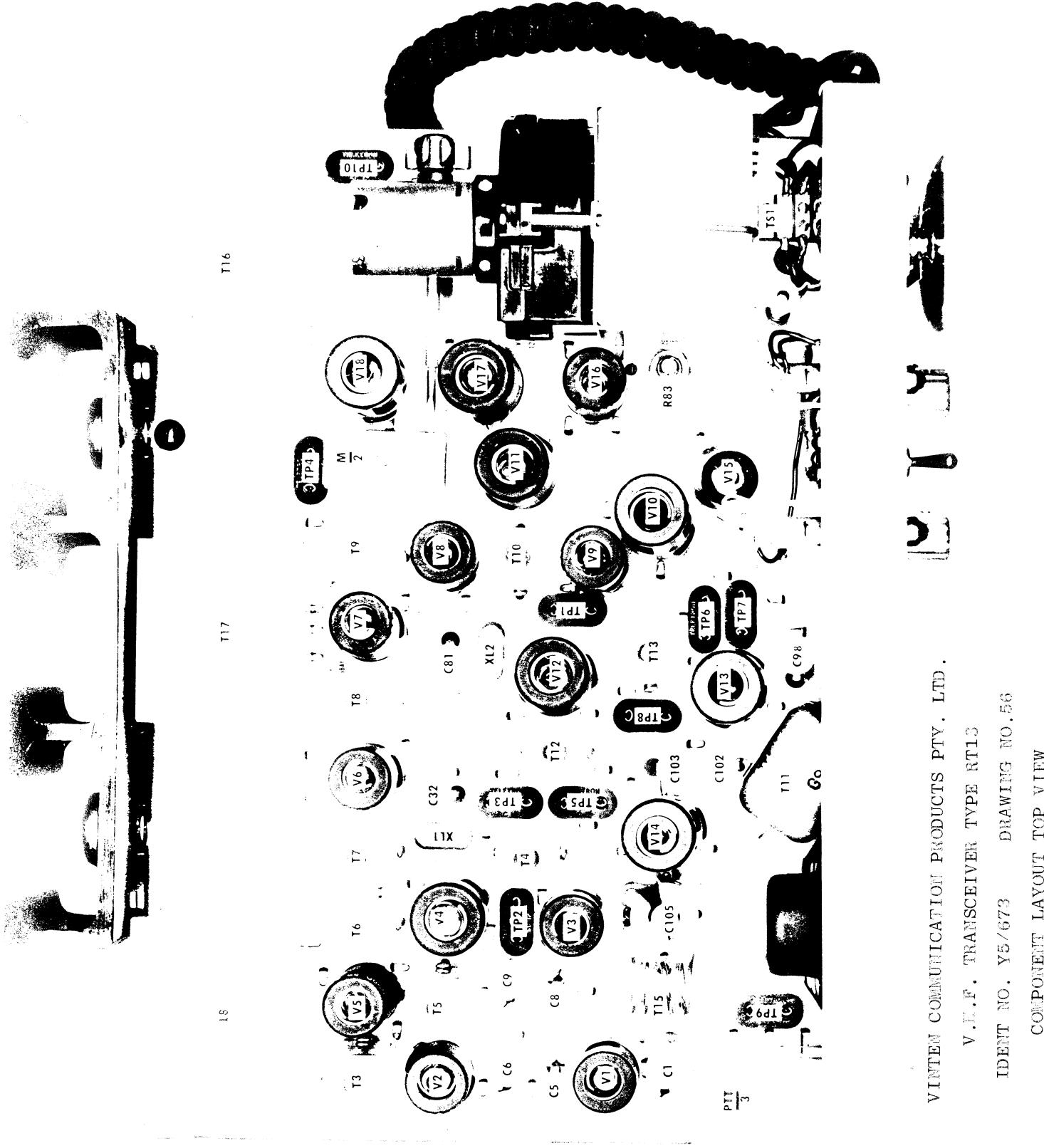
V.H.F. TRANSCEIVER TYPE RT12

IDENT NO. Y5/672

DRAWING NO. 54

COMPONENT LAYOUT TOP VIEW





VINTEN COMMUNICATION PRODUCTS PTY. LTD.

V.T.F. TRANSCEIVER TYPE RT13

IDENT NO. Y5/673 DRAWING NO. 56

COMPONENT LAYOUT TOP VIEW

